



23 developed 32-path CT-TDLAS demonstrated its feasibility of 2D temperature  
24 measurement. 32-path CT-TDLAS was applied to CH<sub>4</sub> and 5 kg/h coal combustion  
25 fields for 2D temperature measurement. The time-series 2D temperature distribution in  
26 coal combustion furnace was measured using 32-path CT-TDLAS measurement cell  
27 with kHz time resolution. The transient temperature field of combustion flame directly  
28 reflects the combustion mode and combustion stability. The measurement results  
29 demonstrate its applicability of CT-TDLAS to various types of combustor, especially  
30 the combustion fields with coal and ash particles. CT-TDLAS method with kHz  
31 response time enables the real-time 2D temperature measurement to be applicable for  
32 combustion analysis.

33 **Keywords:** Coal combustion; 2D temperature measurement; Time-series distribution;  
34 Tunable diode laser absorption spectroscopy (TDLAS); Computed tomography (CT)

## 35 **1. Introduction**

36 The fossil fuel, such as coal, oil and natural gas, is the major source of energy. The  
37 energy and environment issues have become a global concern. The long-term energy  
38 consumption is dominated by coal in China. The safety, high-efficiency and low  
39 pollution are significant for coal combustion. Therefore, investigation of combustion  
40 phenomena in pulverized coal flames is important for combustion optimization with the  
41 development of efficient coal burners and improvement of numerical simulation models.  
42 However, the acquisition of vital combustion parameters is the key to combustion  
43 optimization. The temperature distribution is closely related to the combustion  
44 efficiency, gas pollutants emission, unburned carbon loss, and so on. Especially, real-

45 time two dimensional (2D) temperature and species concentration distributions play an  
46 important role for combustion field analysis. Traditional contact measurement methods  
47 can not realize real-time online monitoring due to some limitations of temperature range,  
48 distribution point, etc.

49 Recently, laser diagnosis has been developed and applied for actual industrial  
50 fields due to its features of non-contact, high sensitivity and fast response [1,2]. Tunable  
51 diode laser absorption spectroscopy (TDLAS) has been developed for temperature and  
52 species concentration measurement in gas turbine, coal gasifier, process control and  
53 environment monitoring using absorption spectra of molecules such as H<sub>2</sub>O, NH<sub>3</sub> and  
54 CH<sub>4</sub> [3-6]. With engineering development, the transient phenomena of start-ups and  
55 load changes in engines have been elucidated in various conditions gradually [7]. A  
56 chemical species tomography scheme, which was amenable to replication for many  
57 simultaneous measurement channels, was applied for simultaneous measurement of  
58 multiple species [8]. The combination method of computed tomography-tunable diode  
59 laser absorption spectroscopy (CT-TDLAS) based on computed tomography (CT) and  
60 TDLAS has also been developed for 2D temperature and species concentration  
61 measurement in automotive engine and aero-propulsion engine [9-11]. Various  
62 tomographic reconstruction methods have been investigated. 2D temperature and NH<sub>3</sub>  
63 concentration were measured using a cylindrical retro-reflector with the algebraic  
64 reconstruction technique (ART) [12]. The hyperspectral absorption spectroscopy  
65 method was developed to increase spectral information for simultaneous reconstruction  
66 of temperature and species concentration [13-15]. In order to simultaneously retrieve

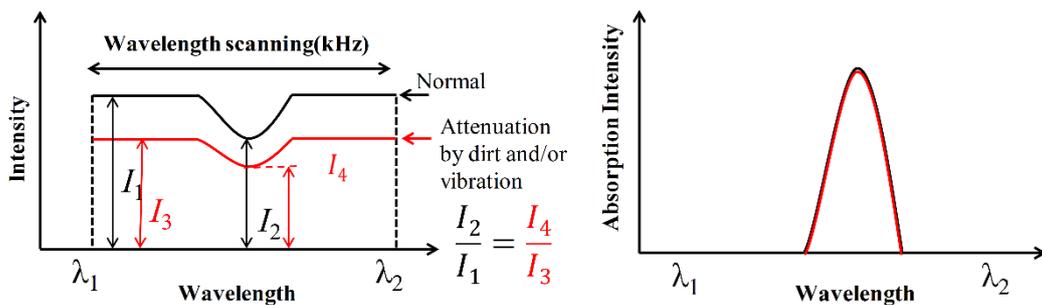
67 distributions of temperature, species concentration and pressure, a technique based on  
68 broad bandwidth and frequency-agile tomographic absorption spectroscopy was also  
69 proposed for the study of dynamic combustion flows [16]. The 16-path CT-TDLAS  
70 method was applied to the oscillating flames and Bunsen type burner for time-series  
71 2D temperature and CH<sub>4</sub> concentration distributions [17,18]. Various spatial resolution  
72 quantification approaches have also been discussed to evaluate the spatial resolution  
73 [19]. Due to the kHz response time of CT-TDLAS, the method enables real-time 2D  
74 temperature and species concentration measurement, which is applicable for the  
75 combustion analysis. However, it has been still difficult to accomplish in-situ  
76 measurement of temperature and species concentration in coal combustion fields  
77 because of the existing coal and ash particles in combustion fields.

78 In this study, a fast response 2D temperature and concentration measurement  
79 method was developed and applied to coal combustion field. The technique is based on  
80 a CT method using absorption spectra of H<sub>2</sub>O molecule. The CT-TDLAS method using  
81 32-path configuration was applied to measure time-series 2D temperature distribution  
82 in a 5 kg/h pulverized coal furnace for the first time. The novel CT algorithm using 2D  
83 polynomials for temperature and concentration distributions was developed to improve  
84 CT reconstruction performance. According to the 2D temperature measurement results,  
85 the coal combustion can be analyzed. The CT-TDLAS application for time-series 2D  
86 temperature measurement in coal combustion field demonstrates its applicability for  
87 severe environment, such as high temperature, high dust, high moisture, corrosivity,  
88 etc.

89 **2. Theory**

90 2.1 CT-TDLAS

91 Gas temperature and species concentration can be determined according to the  
92 measurement of molecular absorbance at multiple wavelengths using TDLAS, which  
93 is possible to scan laser wavelength continuously and detect absorption spectra. TDLAS  
94 technique is based on Lambert Beer's law. The intensity of permeated light is related to  
95 absorber concentration when laser light permeates an absorption medium [1]. The  
96 direct absorption spectroscopy was employed using kHz wavelength scanning, which  
97 shows more distinct spectral evaluation than that of sinusoidal modulation. Figure 1  
98 shows the concept of direct absorption spectroscopy at different conditions. When the  
99 laser intensity is attenuated by dirt on windows, vibration, and/or scattering by particles,  
100 the absorption intensity can be normalized by the laser intensity measured in each  
101 wavelength scanning. The laser intensity fluctuation does not affect the accuracy of  
102 measurement and it is often called “self-calibration” [1]. Temperature can be measured  
103 by evaluating several absorption lines from same molecule with different temperature  
104 dependence [18,20], which is also important to reduce the temperature error induced by  
105 CT algorithm. In this study, H<sub>2</sub>O absorption spectra around 1388nm and 1343nm were  
106 used to measure the temperature.



108 (a) Wavelength scanning (b) Absorption intensity

109 Figure 1 Concept of direct absorption spectroscopy

110 The absorption signal intensity of transmitted light through absorption medium  
111 becomes an integrated value along the optical path. Various optical paths can be  
112 intersected to each other to configurate the optical grids for 2D distribution  
113 reconstruction by a CT method. 32-path laser beams configuration and its 32-path CT  
114 algorithm were used to measure 2D temperature distribution in this study. Concept of  
115 laser beam paths and CT algorithm flow chart is shown in Figure 2. The integrated  
116 absorbance of  $A_{\lambda,p}$  depends on both temperature and concentration. Therefore, the  
117 temperature should be calculated by more than two different absorbance values. In this  
118 study, the theoretical H<sub>2</sub>O spectroscopic database [21] has been corrected under various  
119 temperature and pressure conditions to improve its measurement accuracy. A set of  
120 measured H<sub>2</sub>O absorption spectra is compared to the theoretical spectra with the  
121 corrected spectroscopic database. In order to minimize the spectra fitting error, the  
122 temperature and H<sub>2</sub>O concentration at each analysis position are determined using a  
123 multi-function minimization method. Sets of temperature and concentration  
124 distributions at analysis position can be determined simultaneously shown in Figure 2.  
125 The set of temperature and concentration is determined to minimize the total error,  
126 which is evaluated by the spectra fitting method. A polynomial noise reduction  
127 technique is also used to reduce noises such as the effect of laser beam steering [7]. The  
128 spectra fitting method and polynomial noise reduction technique are significant to  
129 acquire the stable and accurate CT reconstruction.

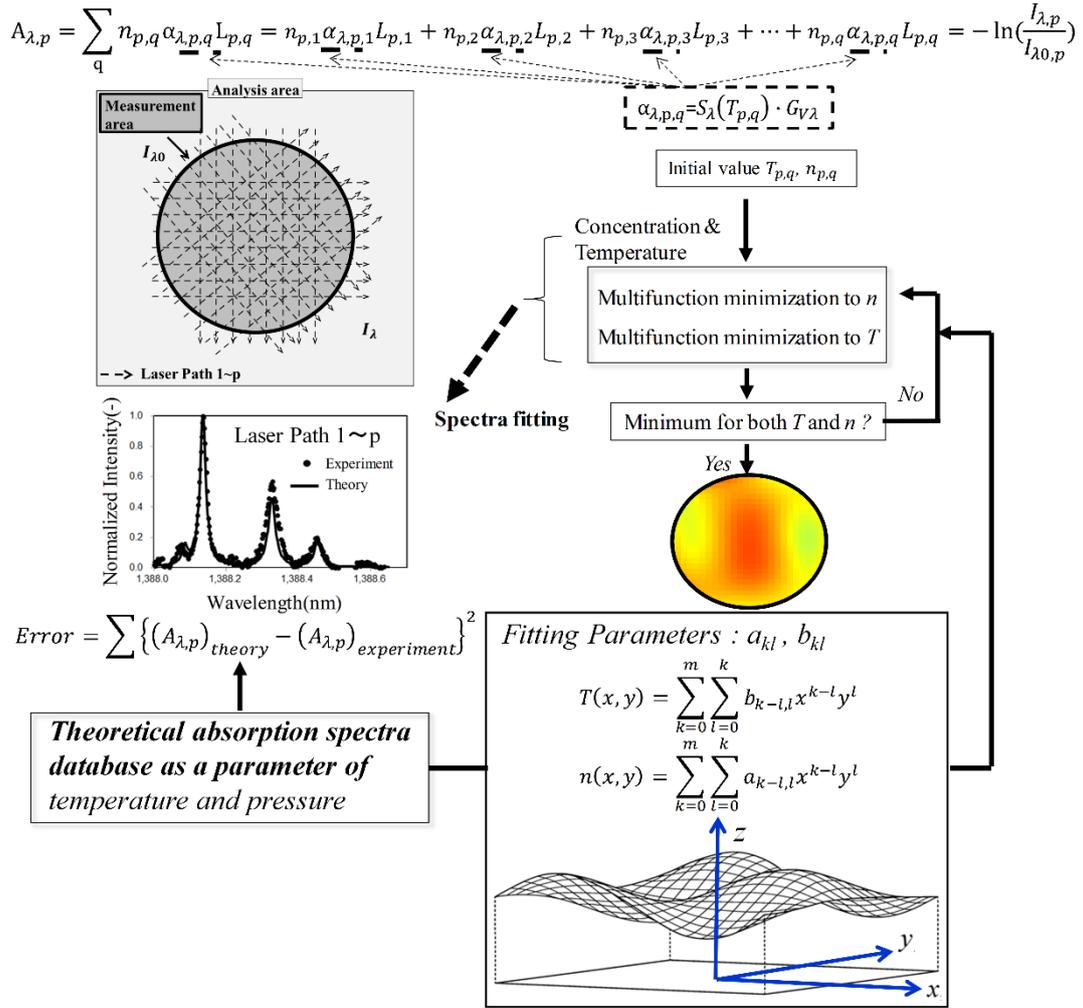


Figure 2 Laser beam paths and CT algorithm

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This novel CT algorithm is developed to realize the stable CT reconstruction calculation. The 2D temperature and concentration distributions are defined by the 2D polynomials for  $T(x,y)$  and  $n(x,y)$  when employing the fitting parameters of  $a_{kl}$  and  $b_{kl}$ . 2D temperature and concentration information is used to calculate the absorption coefficient at each position. The error minimization is performed as a function of the polynomial parameters  $a$  and  $b$ . Using this method, spatial resolution of temperature and concentration distribution can be determined by the polynomial order  $m$  and interval between calculated positions can be minimized arbitrarily. One of the most prominent merits of this method is its stability of reconstruction especially at the edge

141 of measurement area where the laser path number is usually small compared to the  
 142 centre one. This is because the spatial resolution of temperature and concentration  
 143 distribution is determined by the polynomial order and is not determined locally by the  
 144 axes of the measurement area. The downhill simplex [22] and Levenberg-Marquardt  
 145 methods for multifunction minimization were used in this study.

## 146 2.2 Image analysis

147 CT-TDLAS can reconstruct a 2D temperature distribution image using the  
 148 absorption spectra. In order to verify the accuracy of CT reconstruction, the sum of  
 149 squared difference (SSD) and zero-mean normalized cross-correlation (ZNCC)  
 150 between the original profile and the CT reconstructed profile are compared and  
 151 analyzed. The approaches were described elsewhere in detail [23,24]. SSD is the area  
 152 range of reconstructed pattern in the image by comparing the sum of squared difference  
 153 between the pixels of specified area and the pixels of target pattern. If the SSD value is  
 154 closer to “0”, the error between original profile and CT reconstructed profile is smaller  
 155 with almost same values of two profiles. ZNCC is a zero-mean normalized cross-  
 156 correlation, which represents a correlation between original profile and CT  
 157 reconstructed profile. If the ZNCC value is closer to “1”, the correlation between two  
 158 profiles is higher with almost same patterns. Equations (1) and (2) define the SSD value  
 159 and ZNCC value.

$$160 \quad SSD = \sqrt{\frac{\sum_{x=0}^{X-1} \sum_{y=0}^{Y-1} \left[ (T_{x,y})_{original} - (T_{x,y})_{CT-TDLAS} \right]^2}{XY}} / T_R \quad (1)$$

$$161 \quad ZNCC = \frac{\sum_{x=0}^{X-1} \sum_{y=0}^{Y-1} \left[ (T_{x,y} - \bar{T})_{original} \cdot (T_{x,y} - \bar{T})_{CT-TDLAS} \right]}{\sqrt{\sum_{x=0}^{X-1} \sum_{y=0}^{Y-1} (T_{x,y} - \bar{T})_{original} \cdot \sum_{x=0}^{X-1} \sum_{y=0}^{Y-1} (T_{x,y} - \bar{T})_{CT-TDLAS}^2}} \quad (2)$$

$$162 \quad \bar{T} = \frac{\sum_{x=0}^{X-1} \sum_{y=0}^{Y-1} T_{x,y}}{XY} \quad (3)$$

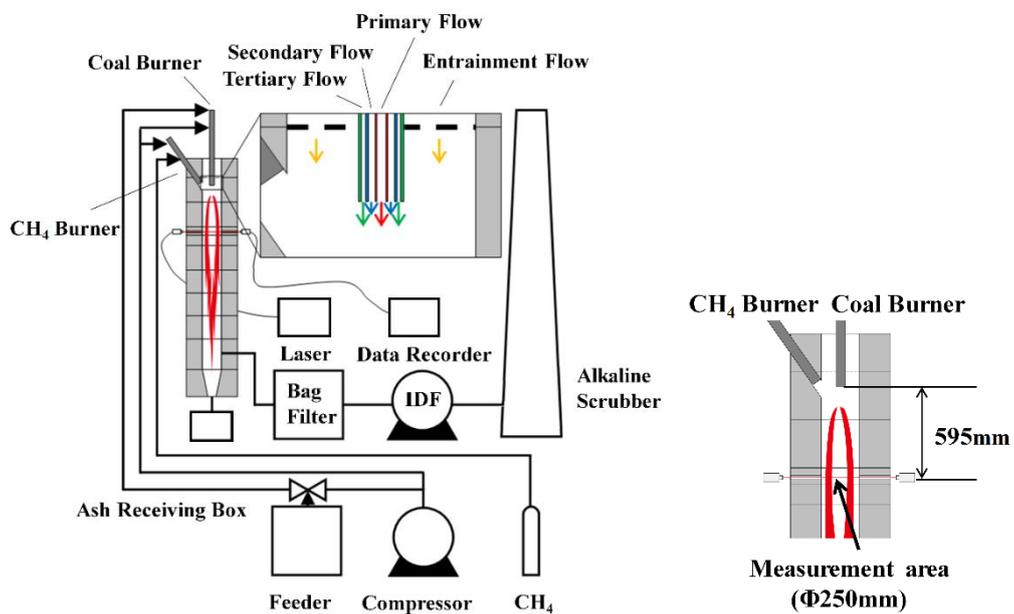
163 Where,  $T_{x,y}$  is the temperature at each position in calculated area.  $T_R$  is the representing  
 164 temperature and was set to be 1800K in this study.  $X$  is the total number of meshes  
 165 along  $x$ -axis in calculated area, and  $Y$  is the total number of meshes along  $y$ -axis in  
 166 calculated area.

167 In this study, the image differences between original profile and its CT  
 168 reconstructed profile were compared to evaluate the CT reconstruction accuracy of  
 169 employed 32-path configuration. The original profiles were simulated by an assumed  
 170 temperature distribution and three computational fluid dynamics (CFD) results.

### 171 **3. Experimental setup**

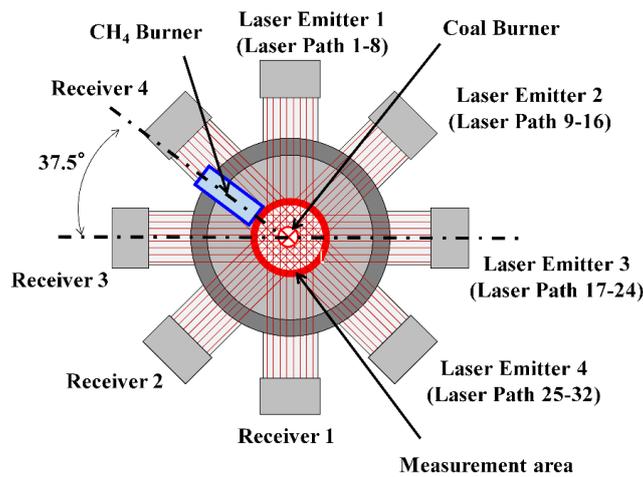
172 CT-TDLAS was applied to pulverized coal combustion furnace with coal feed rate  
 173 of 5 kg/h to measure the time-series 2D temperature distribution in pulverized coal  
 174 flame in this study. Figure 3 shows the experimental apparatus of pulverized coal  
 175 combustion field measurement using CT-TDLAS. The experimental system mainly  
 176 consisted of the combustion furnace with coal burner and pilot methane (CH<sub>4</sub>) burner,  
 177 the CT-TDLAS measurement cell, as well as their related components, as shown in  
 178 Figure 3(a). The combustion furnace was a vertical cylinder with an inner diameter of  
 179 250 mm and height of 2300 mm. The coal burner was a triple concentric jet burner,  
 180 which may become hot because of the radiation from particles. The primary, secondary,

181 and tertiary air were used for feeding coal, protecting coal burner from radiation heat,  
 182 and supplying combustion air, respectively. Inner diameters of the coal burner were 5.7  
 183 mm, 44.6 mm, and 52.5 mm in order. In addition, entrainment air was supplied to  
 184 prevent flowing back. The experimental conditions of CH<sub>4</sub> flame and pulverized coal  
 185 flame were summarized in Table 1. The CT-TDLAS measurement cell was installed at  
 186 the plane of 595 mm from the coal burner inside, as illustrated in Figure 3(b).



(a) Experimental system

(b) Measurement plane



(c) 32-path CT configuration

Figure 3 Experimental apparatus of pulverized coal combustion field measurement using CT-TDLAS

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Table 1 Experimental conditions of CH<sub>4</sub> and pulverized coal flames

	Condition	CH <sub>4</sub> fuel	CH <sub>4</sub> +Coal fuel
Coal burner	Coal feed rate [kg/h]	-----	5
	Primary air flow rate [L <sub>N</sub> /min]	-----	39
	Secondary air flow rate [L <sub>N</sub> /min]	-----	20
	Tertiary air flow rate [L <sub>N</sub> /min]	-----	138
	Entrainment air flow rate [L <sub>N</sub> /min]	-----	198
	Air-fuel ratio [-]	-----	1.1
CH <sub>4</sub> burner	CH <sub>4</sub> flow rate [L <sub>N</sub> /min]	30.0	30.0
	Air flow rate [L <sub>N</sub> /min]	320.0	320.0

194 Temperature measurement using CT-TDLAS was performed using H<sub>2</sub>O  
195 absorption spectra. The wavelengths of diode lasers (NTT Electronics Co.,  
196 NLK1E5GAAA/NLK1B5EAAA) were from 1388.0 to 1388.6 nm and from 1342.9 to  
197 1343.5 nm, which were employed to maintain the sufficient measurement accuracy at  
198 low and high temperature [17,18]. The wavelength scanning rate was 4 kHz. The two  
199 wavelength laser beams were mixed using the fiber combiner and the mixed laser beam  
200 was separated by an optical fiber splitter (OPNETI CO., SMF-28e 1310 nm SWBC  
201 2×32) to 32 paths. The separated laser beams irradiated into the flame by 32 collimators.  
202 The transmitted laser intensities were detected by 32 photodiodes after passing through  
203 the flame and then recorded by analyzer including 32 amplifiers and recorder. In order  
204 to eliminate the radiation effect, the filter (SIGMA KOKI CO., VPF-05C-08P-  
205 T1340/1390-R825/1600) with the transmittance specification of 1340-1390 nm>95%,  
206 500-1250 nm<2%, 1500-2000 nm<2% was utilized with the detectors. As optical access  
207 ports, 32 collimators and 32 detectors were embedded in the 32-path CT-TDLAS  
208 measurement cell. Figure 3(c) shows the designed 32-path CT configuration of  
209 measurement cell with four sets of laser emitters and four sets of receivers. The 32 laser

210 paths in the measurement cell were purged using 40 L<sub>N</sub>/min nitrogen (N<sub>2</sub>) flow to  
211 eliminate H<sub>2</sub>O absorption in the interlayer of measurement cell.

## 212 **4. Results and discussion**

213 32-path CT-TDLAS measurement method for 2D temperature measurement was  
214 used in pulverized coal combustion field. One of the important aspects for CT-TDLAS  
215 application is the accuracy evaluation of CT-TDLAS. Therefore, the accuracy of  
216 employed 32-path CT-TDLAS measurement method was discussed to verify its  
217 reliability before the measurement of 2D temperature distribution of pulverized coal  
218 flame using CT-TDLAS.

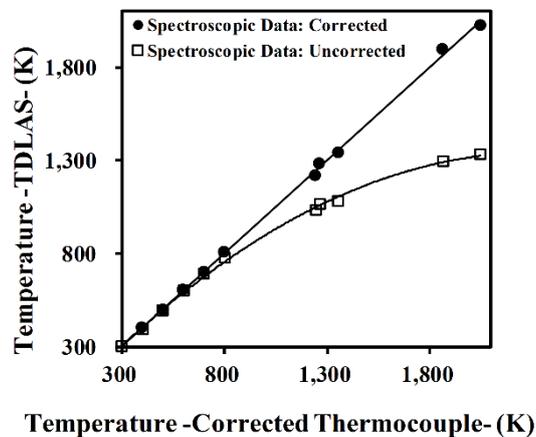
### 219 **4.1 Accuracy evaluation of CT-TDLAS**

220 The accuracy of CT-TDLAS measurement method should be evaluated in two  
221 parts. The temperature measurement accuracy of TDLAS and the 2D reconstruction  
222 accuracy of 32-path CT-algorithm were evaluated respectively in this study.

#### 223 **4.1.1 Accuracy evaluation of TDLAS**

224 In this method, for the temperature measurement using H<sub>2</sub>O absorption spectra,  
225 the theoretical H<sub>2</sub>O spectroscopic database has been corrected under various  
226 temperature and pressure conditions to improve TDLAS measurement accuracy. The  
227 consistency of theoretical absorption spectra and experimental absorption spectra was  
228 improved significantly when employing the corrected spectroscopic database [18,25].  
229 The temperature from 300 to 2000 K of a flat flame burner and a high-temperature and  
230 high-pressure measurement cell was measured by TDLAS and thermocouple to verify  
231 the temperature measurement accuracy of TDLAS [18]. The comparison of measured

232 temperature between TDLAS and thermocouple is shown in Figure 4 and Table 2 under  
233 different temperature conditions. The temperature measured by TDLAS was calculated  
234 using the uncorrected spectroscopic database and corrected spectroscopic database,  
235 respectively. The measured temperature by TDLAS using corrected spectroscopic  
236 database showed the improved linearity with the measured temperature by  
237 thermocouple, as shown in Figure 4. Table 2 lists the temperature difference between  
238 thermocouple and TDLAS with corrected spectroscopic database, which shows that the  
239 maximum difference was 32.5 K and the maximum error was 2.3% in the measured  
240 temperature range from 300 to 2000 K. Therefore, the correction of spectroscopic  
241 database is necessary to improve the temperature measurement accuracy for TDLAS  
242 technique.



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244 Figure 4 Temperature comparison between thermocouple and TDLAS with/without  
245 corrected spectroscopic database  
246

247 Table 2 Temperature difference between thermocouple and TDLAS with corrected  
 248 spectroscopic database

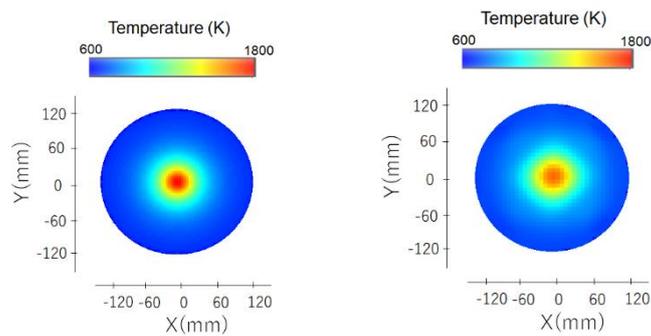
Thermocouple (K)	TDLAS with correction (K)	Temperature difference (K)	Error
300	299.9	-0.1	0.0%
400	398.9	-1.1	0.3%
500	498.9	-1.1	0.2%
600	604.0	4.0	0.7%
700	699.8	-0.2	0.0%
800	803.3	3.3	0.4%
1244	1215.0	-29.0	2.3%
1264	1282.3	18.4	1.5%
1354	1340.0	-14.0	1.0%
1864	1896.5	32.5	1.7%
2048	2021.5	-26.6	1.3%

249 4.1.2 Accuracy evaluation of 32-path CT reconstruction

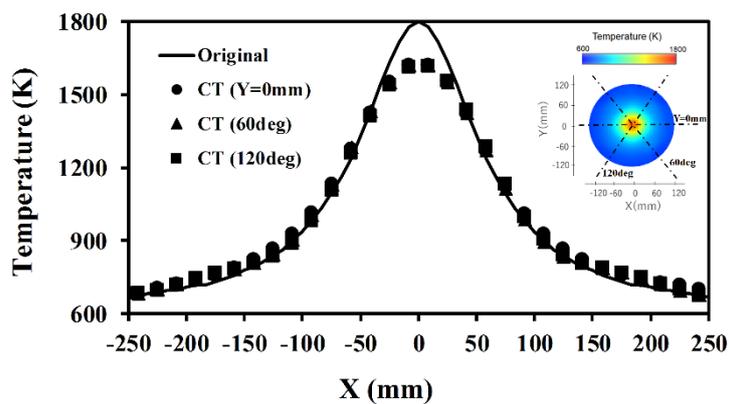
250 The accuracy of CT reconstruction can be evaluated using the assumed  
 251 temperature distribution and/or CFD result of temperature distribution. In this study,  
 252 the image differences given by an assumed temperature profile and its corresponding  
 253 CT reconstructed profile of 32-path configuration were discussed to evaluate the 2D  
 254 reconstruction accuracy of 32-path CT-algorithm. Three CFD results of temperature  
 255 distribution were also used to evaluate the accuracy of 32-path CT reconstruction.

256 An assumed temperature distribution based on centrosymmetric Cauchy  
 257 distribution was used first, as shown in Figure 5(a). Figure 5 shows the comparison  
 258 between the assumed temperature distribution with high temperature region in center  
 259 and its 32-path CT reconstructed result. The reconstructed profile shows the accordant  
 260 temperature distribution with the original profile according to Figure 5(a) and Figure  
 261 5(b). The temperature distributions at Y=0mm, 60deg and 120deg were compared  
 262 between original distribution and CT reconstructed results, which shows some  
 263 difference at the region around X=Y=0mm in Figure 5(c). Because of the limited

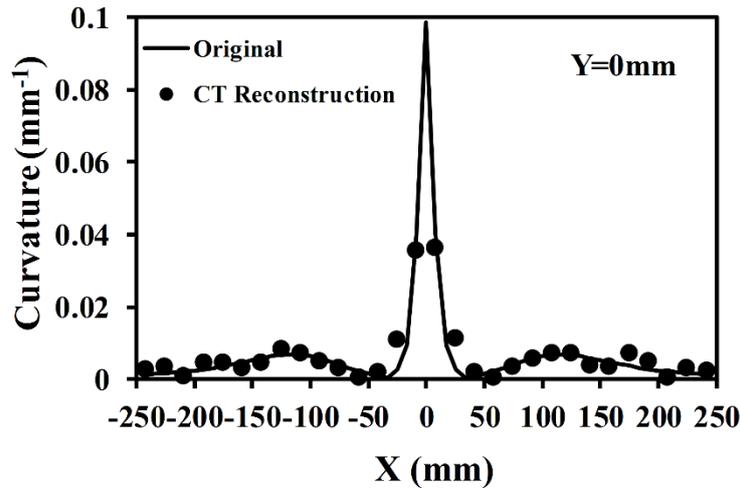
264 number of paths, the temperature change with large curvature cannot be reconstructed  
 265 correctly by the employed 32-path configuration. The accuracy of CT reconstruction  
 266 can be improved when increasing the paths, which depends on the actual situation of  
 267 applications. Figure 5(d) shows the comparison of curvature at  $Y=0\text{mm}$ . The maximum  
 268 curvature of the CT reconstructed result was  $0.04\text{ mm}^{-1}$ . If the spatial resolution was  
 269 defined using the radius of curvature, the spatial resolution of this method was  
 270 determined to 25 mm. The spatial resolution can be improved when increasing the laser  
 271 path. If using 64 paths, the spatial resolution becomes to be 12 mm evaluated by the  
 272 maximum curvature.



273 (a) Assumed temperature 1 (b) CT reconstruction 1



275 (c) Comparison of temperature distributions at  $Y=0\text{mm}$ , 60deg and 120deg



(d) Comparison of curvature at Y=0mm

Figure 5 Comparison of temperature distributions between assumed temperature and reconstructed temperature by 32-path CT-algorithm

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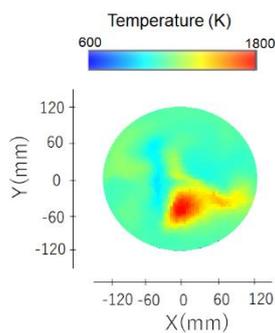
294

A numerical simulation of a pulverized coal flame for temperature distribution was performed with working model sets by Large Eddy Simulation (LES) technique using NuFD/FrontFlowRed (FFR-Comb). The employed gas-particle two-phase reacting flow LES solver was unstructured and based on Finite Volume Method (FVM) with massively parallel computing code. The turbulence model and combustion model were dynamic Smagorinsky and scale similarity filtered reaction rate models for flow field. As for particle motion, coal particles were traced in the Lagrangian method individually. The field model was employed as the combustion model. The boundary condition was adiabatic for simulation. The detailed description of pulverized coal combustion simulation was reported elsewhere [26-28]. These simulated temperature distributions were also reconstructed according to the 32-path configuration. Figure 6 shows the comparison between three CFD temperature distributions and their CT reconstructions. These results were good enough to be considered as almost the same profiles. Therefore, it is demonstrated that the CT reconstructed distribution in the measured area agreed

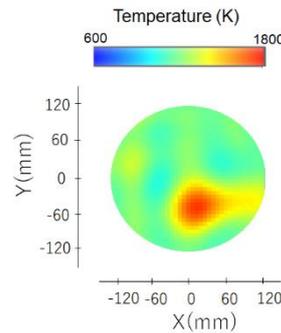
295 well with the original distribution. In Figure 5 and Figure 6, the CT reconstructed  
 296 distributions spread more widely than these of the assumed and CFD distributions due  
 297 to the calculation of CT reconstruction based on limited number of absorbance. Table  
 298 3 lists SSD and ZNCC for these four reconstructed cases. The SSD value is closer to  
 299 “0” and the ZNCC value is closer to “1”, which demonstrate smaller error and higher  
 300 correlation of two profiles. SSD and ZNCC in Table 3 show reasonable results to verify  
 301 the CT reconstruction accuracy.

302 **Table 3 SSD and ZNCC of 32-path CT-algorithm**

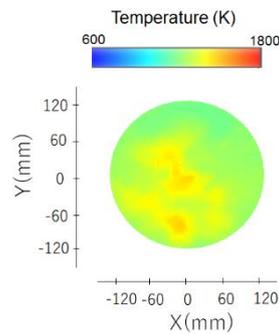
	SSD	ZNCC
Assumed temperature 1	0.018	0.993
CFD temperature 2	0.046	0.925
CFD temperature 3	0.044	0.927
CFD temperature 4	0.043	0.955



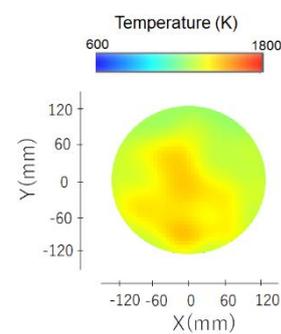
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304 (a) CFD temperature 2



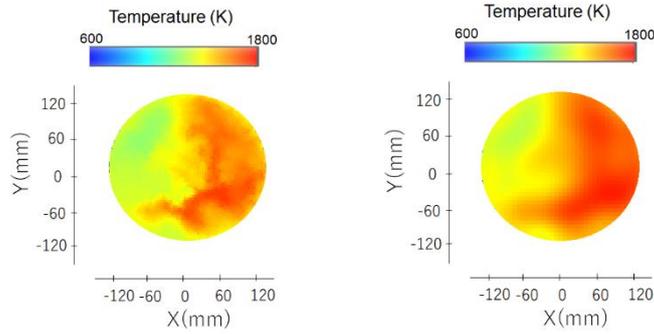
(b) CT reconstruction 2



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306 (c) CFD temperature 3



(d) CT reconstruction 3



(e) CFD temperature 4 (f) CT reconstruction 4

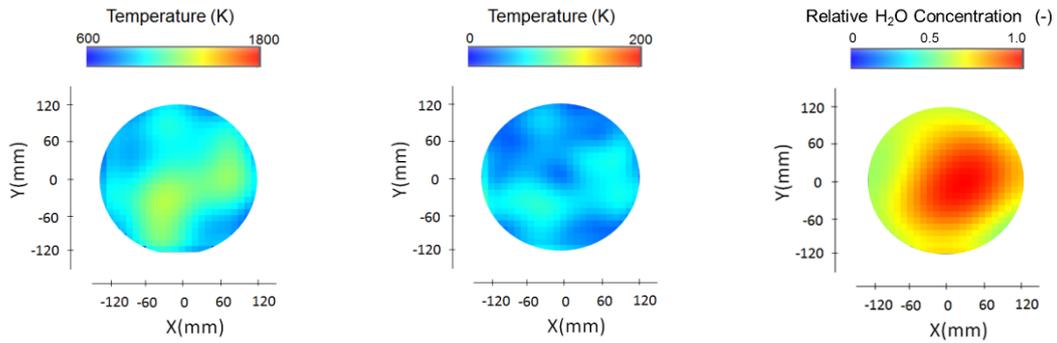
Figure 6 Comparison of CFD temperature distributions and their reconstructed temperature distributions by 32-path CT-algorithm

#### 4.2 Measurement of pulverized coal combustion using 32-path CT-TDLAS

The above reliable validation of CT-TDLAS demonstrated the feasibility of 2D temperature measurement using 32-path CT-TDLAS. Therefore, 2D temperature distribution in the pulverized coal combustion field was measured using this developed 32-path CT-TDLAS. According to the 32-path configuration, the 2D temperature distribution was plotted using  $39 \times 39$  pixels (6mm resolution).

Two combustion states of  $\text{CH}_4$  flame and pulverized coal flame were measured and discussed. Table 1 lists the experimental conditions for each combustion state. The  $\text{CH}_4$  flow and air flow were introduced into  $\text{CH}_4$  burner for  $\text{CH}_4$  flame measurement in the combustion furnace. In the case of pulverized coal flame measurement, the fuels of  $\text{CH}_4$  and pulverized coal were introduced into  $\text{CH}_4$  burner and coal burner for combustion.  $\text{CH}_4$  was used as a pilot gas for ignition and combustion. The  $\text{CH}_4$  flame and pulverized coal flame were measured using 32-path CT-TDLAS respectively. 480 data, which were 480 ms time-series 2D temperature data, were analyzed in each flame condition. Figures 7 and 8 show the measured 2D temperature distribution and relative  $\text{H}_2\text{O}$  concentration distribution of  $\text{CH}_4$  flame and pulverized coal with  $\text{CH}_4$  flame.  $\text{H}_2\text{O}$

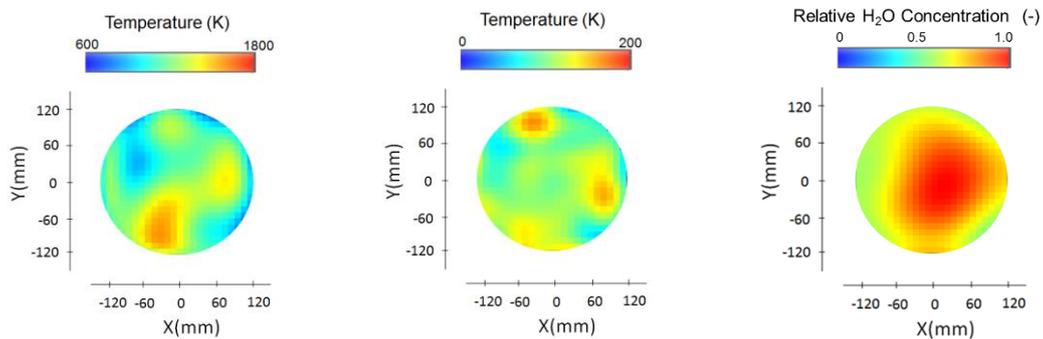
327 concentration distribution was normalized by the maximum H<sub>2</sub>O concentration  
328 distribution in each flame. The temperature distributions at the measurement plane can  
329 be reconstructed and observed, which illustrated different temperature distributions in  
330 CH<sub>4</sub> flame and pulverized coal flame. When comparing the average temperature  
331 distributions in Figure 7(a) and Figure 8(a), the temperature was higher in pulverized  
332 coal flame. These results indicate that the temperature increased when feeding coal to  
333 furnace. The input heat increased with the coal feed compared with that of only CH<sub>4</sub>.  
334 Additionally, Figure 7(b) and Figure 8(b) show the temperature standard deviation of  
335 480 data for CH<sub>4</sub> flame and pulverized coal flame. The standard deviation of  
336 temperature also increased with the coal feed and became large in the region with large  
337 temperature gradient. The combustion characteristic of gas fuel and pulverized coal are  
338 different due to the effect of component, morphology and so on. The combustion  
339 processes of pulverized coal usually consist of volatile devolatilization and combustion,  
340 carbon particles combustion after devolatilization, which are much more complex than  
341 that of CH<sub>4</sub> combustion. The temperature fluctuation of pulverized coal flame was  
342 larger because of coal particle effect including these combustion processes. One of the  
343 merits of CT-TDLAS method is the simultaneous measurement of temperature and  
344 concentration. 2D distributions of relative H<sub>2</sub>O concentration in CH<sub>4</sub> flame and  
345 pulverized coal flame were reconstructed, as shown in Figure 7(c) and Figure 8(c).



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347 (a) Average temperature (b) Standard deviation (c) Relative H<sub>2</sub>O concentration

348 Figure 7 Temperature and relative H<sub>2</sub>O concentration distributions of CH<sub>4</sub> flame



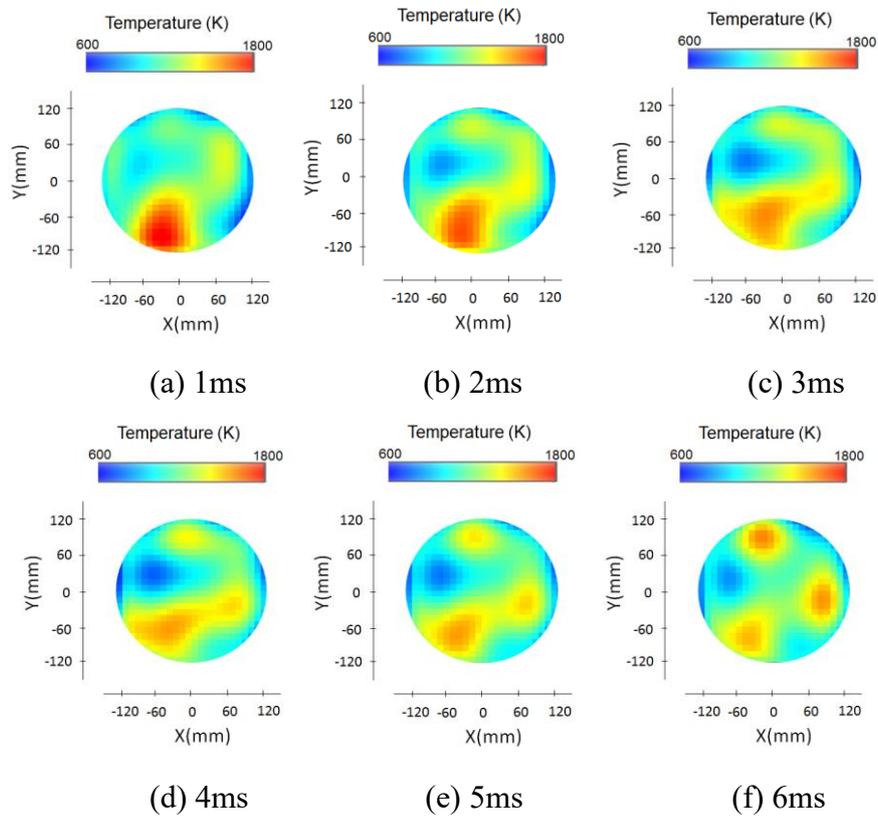
349

350 (a) Average temperature (b) Standard deviation (c) Relative H<sub>2</sub>O concentration

351 Figure 8 Temperature and relative H<sub>2</sub>O concentration distributions of pulverized coal  
352 flame

353 The time-series 2D temperature distribution was also detected with kHz time  
354 resolution. Time-series temperature distribution of pulverized coal flame is shown in  
355 Figure 9. The flame evolution of ms time scale was detected successfully in a turbulent  
356 coal combustion field. The variation of 2D temperature distribution can be investigated  
357 at different instants of time. The transient temperature field of combustion flame  
358 directly reflects the combustion mode and combustion stability. Due to the diversity,  
359 inhomogeneity, composition complexity of coal, the combustion laws of pulverized  
360 coal in coal combustion furnace can be further understood according to these  
361 measurement results. Simultaneity, the combustion furnace will be controlled in real  
362 time when the time-series temperature distribution is combined with combustion  
363 optimization and control strategy. The current results demonstrate that 2D temperature

364 distribution of pulverized coal flame can be detected using 32-path CT-TDLAS, which  
365 shows CT-TDLAS applicability to dusty combustion fields in real time for combustion  
366 phenomena investigation.



369  
370  
371 Figure 9 Time-series 2D temperature distribution of pulverized coal flame

## 372 5. Conclusions

373 It is of great importance to diagnose and control combustion process for coal  
374 combustion in real time. The 2D temperature measurement method using CT-TDLAS  
375 was developed for a pulverized coal combustion furnace. The temperature measurement  
376 accuracy of TDLAS using H<sub>2</sub>O absorption spectra and the 2D reconstruction accuracy  
377 of developed 32-path CT-algorithm were evaluated to verify its reliability for 2D  
378 temperature measurement. The contrast analysis for measured results of average  
379 temperature and temperature standard deviation between CH<sub>4</sub> flame and pulverized  
380 coal flame proved the complexity of pulverized coal combustion. The time-series 2D

381 temperature distribution was successfully reconstructed with ms time scale in the  
382 pulverized coal combustion conditions. It is demonstrated that this CT-TDLAS method  
383 enables the real-time 2D temperature measurement in dusty combustion fields such as  
384 coal burners. Potential extension of this research in the future is to investigate a  
385 monitoring and control system coupled with laser measurement and numerical  
386 simulation for combustion diagnostics.

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